Standard approach

- (1) Convert the digital filter specifications into an analogue prototype lowpass filter specifications
- (2) Determine the analogue lowpass filter transfer function  $H_a(s)$
- (3) Transform  $H_a(s)$  by replacing the complex variable to the digital transfer function

• This approach has been widely used for the following reasons:

(1) Analogue approximation techniques are highly advanced

- (2) They usually yield closed-form solutions
- (3) Extensive tables are available for analogue filter design
- (4) Very often applications require digital simulation of analogue systems

• Let an analogue transfer function be

$$H_a(s) = \frac{P_a(s)}{D_a(s)}$$

- where the subscript "a" indicates the analogue domain
- A digital transfer function derived from this is denoted as

$$G(z) = \frac{P(z)}{D(z)}$$

- Basic idea behind the conversion of  $H_a(s)$  into G(z) is to apply a mapping from the *s*-domain to the *z*-domain so that essential properties of the analogue frequency response are preserved
- Thus mapping function should be such that
  - Imaginary  $(j\Omega)$  axis in the *s*-plane be mapped onto the unit circle of the *z*-plane
  - A stable analogue transfer function be mapped into a stable digital transfer function

# IIR Digital Filter: The bilinear transformation

- To obtain G(z) replace s by f(z) in H(s)
- Start with requirements on *G*(*z*)

<u>G(Z)</u>	<u>Available <i>H</i>(<i>s</i>)</u>
Stable	Stable
Real and Rational in z	Real and Rational in <i>s</i>
Order <i>n</i>	Order <i>n</i>
L.P. (lowpass) cutoff $\Omega_c$	L.P. cutoff $\omega_c T$

## **IIR Digital Filter**

 Hence f(z) is real and rational in z of order <u>one</u>

• i.e. 
$$f(z) = \frac{az+b}{cz+d}$$

• For LP to LP transformation we require

$$s = 0 \rightarrow z = 1 \quad f(1) = 0 \rightarrow a + b = 0$$
  
$$s = \pm j \infty \rightarrow z = -1 \quad f(-1) = \pm j \infty \rightarrow c - d = 0$$

• Thus  $f(z) = \left(\frac{a}{c}\right) \cdot \frac{z-1}{z+1}$ 

## **IIR Digital Filter**

• The quantity  $\left(\frac{a}{c}\right)$  is fixed from  $\omega_c T \leftrightarrow \Omega_c$ 

• ie on  

$$C:|z|=1$$
  $f(z)|_c = \left(\frac{a}{c}\right) \cdot j \tan \frac{\omega T}{2}$ 

• Or  

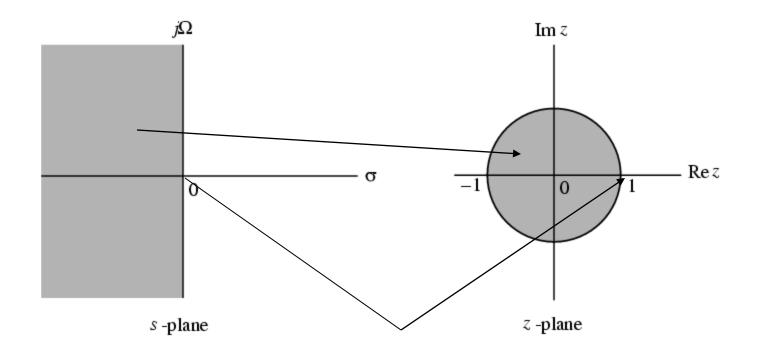
$$j\Omega_c = \left(\frac{a}{c}\right) j \tan \frac{\omega_c T}{2}$$
  
• and  
 $s = \left(\frac{\Omega_c}{\tan\left(\frac{\omega_c T}{2}\right)}\right) \frac{1-z^{-1}}{1+z^{-1}}$ 

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 Transformation is unaffected by scaling. Consider inverse transformation with scale factor equal to unity

•	For $z = \frac{1+s}{1-s}$
	$s = \sigma_o + j\Omega_o$
•	$z = \frac{(1 + \sigma_o) + j\Omega_o}{(1 - \sigma_o) - j\Omega_o} \implies  z ^2 = \frac{(1 + \sigma_o)^2 + \Omega_o^2}{(1 - \sigma_o)^2 + \Omega_o^2}$ and so
	$\sigma_o = 0 \rightarrow  z  = 1$
	$\sigma_o < 0 \rightarrow  z  < 1$
	$\sigma_o > 0 \rightarrow  z  > 1$

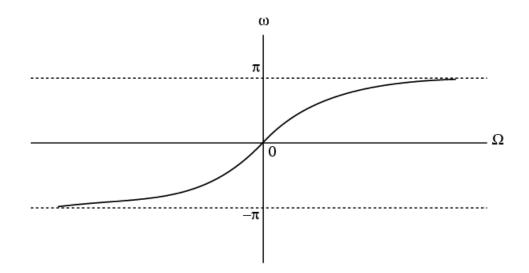
• Mapping of *s*-plane into the *z*-plane



• For  $z = e^{j\omega}$  with unity scalar we have

$$j\Omega = \frac{1 - e^{-j\omega}}{1 + e^{-j\omega}} = j\tan(\omega/2)$$





- Mapping is highly nonlinear
- Complete negative imaginary axis in the *s*plane from  $\Omega = -\infty$  to  $\Omega = 0$  is mapped into the lower half of the unit circle in the *z*-plane from z = -1 to z = 1
- Complete positive imaginary axis in the *s*plane from  $\Omega = 0$  to  $\Omega = \infty$  is mapped into the upper half of the unit circle in the *z*-plane from z = 1 to z = -1

### **Spectral Transformations**

- To transform  $G_L(z)$  a given lowpass transfer function to another transfer function  $G_D(\hat{z})$ that may be a lowpass, highpass, bandpass or bandstop filter (solutions given by Constantinides)
- $z^{-1}$  has been used to denote the unit delay in the prototype lowpass filter  $G_L(z)$  and  $\hat{z}^{-1}$ to denote the unit delay in the transformed filter  $G_D(\hat{z})$  to avoid confusion

### **Spectral Transformations**

• Unit circles in z- and  $\hat{z}$  -planes defined by

$$z = e^{j\omega}, \qquad \hat{z} = e^{j\hat{\omega}}$$

• Transformation from *z*-domain to

 $\hat{z}\,$  -domain given by

$$z = F(\hat{z})$$

Then

$$G_D(\hat{z}) = G_L\{F(\hat{z})\}$$